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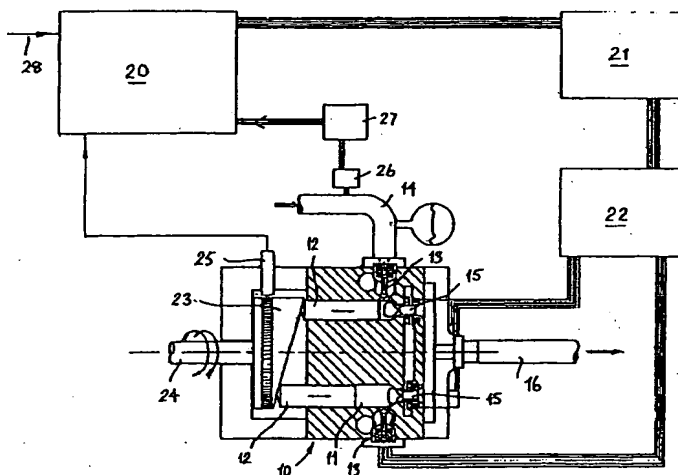
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[Continued on next page]

- (54) Title: FLUID-WORKING MACHINE AND OPERATING METHOD



- (57) Abstract: A fluid-working machine has a plurality of working chambers, e.g. cylinders (11), of cyclically changing volume, a high-pressure fluid manifold (14) and a low-pressure fluid manifold (16), at least one valve (13, 15) linking each working chamber to each manifold, and electronic sequencing means (20) for operating said valves in timed relationship with the changing volume of each chamber (11), wherein the electronic sequencing means is arranged to operate the valves of each chamber in one of an idling mode, a partial mode in which only part of the usable volume of the chamber is used, and a full mode in which all of the usable volume of the chamber (11) is used, and the electronic sequencing means (20) is arranged to select the mode of each chamber on successive cycles so as to infinitely vary the time averaged effective flow rate of fluid through the machine.

**Declarations under Rule 4.17:**

- as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii)) for the following designations AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GI, GM, II, IU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PI, PT, RO, RU, SC, SD, SE, SG, SK, SI, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VC, VN, YU, ZA, ZM, ZW, ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU,

TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO, SE, SI, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG)

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FLUID-WORKING MACHINE AND OPERATING METHOD

Background to the Invention

5 This invention relates to a fluid-driven (motor) and/or fluid-driving (pump) machine having a plurality of working chambers of cyclically changing volume and valve means to control the connection of each chamber to low- and high-pressure manifolds. The invention also relates to a method of operating the machine.

10 The invention has particular reference to non-compressible fluids, but its use with gases is not ruled out. It has particular reference to machines where the at least one working chamber comprises a cylinder in which a piston is arranged to reciprocate, but its use with at least one chamber delimited by a flexible diaphragm or a rotary piston is not ruled out.

15 With most fluid working machines the fluid chambers undergo cyclical variations in volume following a sinusoidal function. It is known to provide flow rectifying seating valves, allowing fluid to be admitted and exhausted from the working chamber, which valves are electro-magnetically actuated such that pumping and motoring strokes can be achieved. The chamber can be left to idle by holding the
20 valve, between the working chamber and the low-pressure sump, in the open condition.

A shaft position sensor is used to provide the micro-controller with chamber phase information while flow or pressure demand inputs influence the rate at which chambers are pumped, motored or left idle. The micro-controller drives semiconductor
25 switches, such as field effect transistors, which in turn actuate the valves connecting the chambers to either the high-pressure manifold or low-pressure sump.

Experience shows that varying the timing of the valves, such that portions of the stroke are disabled, in order to vary machine output creates a significant amount of
30 audible and fluid borne noise.

The development of electro-magnetically actuated, seating valves working in conjunction with a varying fluid chamber volume, such as described in EP-A-361927 and EP-A-0494236, permitted the output of a fluid working machine having a plurality of working chambers to be varied, in a time averaged way, by the rate of selection of whole chambers as they became available at the ends of each expansion or contraction cycle.

EP-A-0361927 described the use of this technique for a pump in which shaft power was controllably converted to fluid power. EP-A-0494236 continued the concept and, by introducing a new mechanism for actuating the valves in a motoring cycle, developed the machine to allow a controllable bi-directional energy flow.

A multi-piston hydraulic machine according to EP-A-0494236 is shown in schematic section in Figure 1. In the side wall of each cylinder 11 is a poppet valve 13 communicating with a high-pressure manifold 14 and in the end wall of each cylinder is a poppet valve 15 communicating with a low-pressure manifold 16. The poppet valves 13 and 15 are active electromagnetic valves controlled electrically by a microprocessor controller 20 feeding control signals, via optoisolators 21, to valve-driving semiconductors 22.

Pistons 12 act on a drive cam 23 fast to an output shaft 24, the position of the cam 23 being sensed by an encoder 25.

The controller 20 receives inputs from the encoder 25, a pressure transducer 26 (via an analogue to digital converter 27) and via a line 28 to which a desired output speed demand signal can be applied.

The poppet valves 13, 15 seal the respective cylinders 11 from the respective manifolds 14, 16 by engagement of an annular valve part with an annular valve seat, a solenoid being provided to magnetically move each said valve part relative to its seat by reacting with ferromagnetic material on the said poppet valve, each said poppet

valve having a stem and an enlarged head, the annular valve part being provided on the head and the ferromagnetic material being provided on the stem.

5 In EP-A-361927 and EP-A-0494236, whole chambers were selected on the basis that valve actuation could be done during the instances of near zero flow. It was considered that delayed closure of valves, occurring during times of significant flow, such that part of the chamber displacement could be rejected, would result in extremely high rates of change of flow and pressure, which in turn would generate noise.

10 The approach of whole chamber selection works well for high flow rates, seeing as the mechanical payload, driven by this type of system, typically has a large momentum such that variations in flow energy cause relatively small changes in its velocity and, therefore, acceleration.

15 However, in practice it was found that whole chamber selection during times of low flow demand resulted in large flow variations, seeing as the fluid machine was idle for long instances between active chambers. When a payload has a small velocity, as it will when the actuating flow is low, the momentum will also be minimal. If each actuated chamber is considered to be delivering a quantum of energy to the payload,
20 then the change in velocity will be significantly higher when the initial energy is low.

Summary of the Invention

The invention seeks to address this problem such that a smooth actuating response can be achieved at the payload.

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The present invention provides a fluid-working machine having a plurality of working chambers of cyclically changing volume, a high-pressure fluid manifold and a low-pressure fluid manifold, at least one valve linking each working chamber to each manifold, and electronic sequencing means for operating said valves in timed
30 relationship with the changing volume of each chamber, wherein the electronic sequencing means is arranged to operate the valves of each chamber in one of an idling mode, a partial mode in which only part of the usable volume of the chamber is used,

and a full mode in which all of the usable volume of the chamber is used, and the electronic sequencing means is arranged to select the mode of each chamber on successive cycles so as to vary the time averaged effective flow rate of fluid through the machine.

5

In a most preferred embodiment of the invention, the partial mode comprises the use of only a small fraction of the usable volume of the chamber.

Preferably, the machine is operable as both a pump and a motor, each chamber
10 having five selectable modes, namely idling mode, partial motoring mode, full motoring mode, partial pumping mode and full pumping mode.

Preferably, the working chambers comprise cylinders in which pistons are arranged to reciprocate. If so, the partial pumping mode preferably includes closing the
15 valve linking the cylinder to the low-pressure manifold and opening the valve linking the cylinder to the high-pressure manifold a small fraction in advance of the top dead centre position of the piston. The partial motoring mode preferably includes closing the valve linking the cylinder to the high-pressure manifold and opening the valve linking the cylinder to the low-pressure manifold a small fraction after the top dead centre
20 position of the piston.

If valve actuations are delayed in this way to almost the end of the stroke, then the rate of change of chamber volume will be at an acceptably low level to permit valve actuation. This means that a small fraction of a whole cylinder can also be selected by
25 the controller to add to the machine's output. The range over which this is practicable is limited by stability of valve operation, on the low flow end, and by machine noise on the higher end. In practice this range is sufficiently limited that it is considered to have added two distinct, low-flow, modes to the three-mode machine, providing the above-mentioned range of five modes to the controller at any time that a chamber comes to the
30 position at which an action can be taken.

The invention also provides a method of operating a fluid-working machine having a plurality of working chambers of cyclically changing volume, a high-pressure fluid manifold and a low-pressure fluid manifold, at least one valve linking each working chamber to each manifold, comprising operating the valves of each chamber in one of an idling mode, a partial mode in which only part of the usable volume of the chamber is used, and a full mode in which all of the usable volume of the chamber is used, wherein the mode of each chamber is selected on successive cycles so as to vary the time averaged effective flow rate of fluid through the machine.

10 Preferably, the method comprises selecting the number of chambers to be operated in each of said modes according to an algorithm depending on the actual and required output of the machine.

15 In a most preferred embodiment of the invention, the partial mode comprises the use of only a small fraction of the usable volume of the chamber.

The method may comprise a preliminary step of selecting whether to operate the machine as a pump or a motor, and choosing the algorithm accordingly.

20 Brief Description of the Drawings

In order that the invention may be more readily understood, embodiments thereof will now be described, by way of example only, with reference to the accompanying drawings, in which:

25 Figure 1 is a schematic sectional view of the known fluid-working machine described above which can be adapted according to the present invention;

Figure 2 is a pulse and timing diagram for the adapted machine when operating as a pump; and

30

Figure 3 is a pulse and timing diagram for the adapted machine when operating as a motor.

Detailed Description of Particular Embodiments

The machine described in EP-A-0494236 and shown in Figure 1 can be adapted to provide a machine according to the invention without additional hardware to create a part-stroke mode. The adaptation consists of increasing the functionality and complexity of the microprocessor control algorithms.

At any one instant there are four possible states for any of the chambers 11: (1) intake from the low-pressure manifold, (2) exhaust to the low-pressure manifold, (3) intake from the high-pressure manifold and (4) exhaust to the high-pressure manifold.

Let "mode" denote a repeating cyclic sequence of transitions from one of these states to another. There are five distinct modes: full stroke pumping, part stroke pumping, full stroke motoring, part stroke motoring, and idling.

The difference between full and part stroking modes is the phase angle at which transitions are made from one of these states to the other relative to bottom and top dead centre of piston movement:

Figures 2 and 3 are timing diagrams for pumping and motoring respectively, showing piston position, the states of electronic gates for controlling the high-pressure and low-pressure valves, the positions of those valves and the cylinder pressure, all plotted against time. The shaded portions indicate active portions of the piston stroke.

In the case of full stroke pumping mode, shown at the bottom right of Figure 2, the transition from state (1) to state (4) happens at or near to bottom dead centre causing the full cylinder volume to be pumped into the high-pressure manifold.

In the case of part stroke pumping mode, shown in the top half of Figure 2, the transition from state (1) to state (4) happens a small fraction in advance of top dead centre, causing only a small fraction of the cylinder volume to be pumped into the high-pressure manifold.

In both pumping modes the transition from state (4) to state (1) happens at or near to top dead centre.

5 In the case of full stroke motoring mode, shown in the bottom half of Figure 3, the transition from state (3) to state (2) happens at or near to bottom dead centre, causing the full cylinder volume to be inducted from the high-pressure manifold. The transition from state (2) to state (3) happens at or near to top dead centre.

10 In the case of part stroke motoring mode, shown in the top half of Figure 3, the transition from state (3) to state (1) happens a small fraction after top dead centre, causing only a small fraction of the cylinder volume to be inducted from the high-pressure manifold. The transition from state (1) to state (2) happens at bottom dead centre. The transition from state (2) to state (3) happens at or near to top dead centre of piston movement.

15 In the case of idling mode, shown at the bottom left of Figure 2, the transition from state (1) to state (2) happens at bottom dead centre of piston movement. The transition from state (2) to state (1) happens at top dead centre of piston movement.

20 A sequence of mode changes on successive machine cycles mixing pumping or motoring modes with idling modes allows the time averaged effective flow rate into and out of the high-pressure manifold to be infinitely varied between full pumping flow, zero flow, and full motoring flow.

25 Since the machine has a plurality of chambers, and each chamber may be set in any of five states, then many instantaneous configurations are possible. Some physical limitations exist however, in that a chamber which has been selected for full-stroke operation cannot, on the same part of the cycle, be selected for part-stroke use.

30 Control Over the Full Range of Output

The flow control method described in EP-A-0361927 and EP-A-0494236, which used a displacement demand during an accounting interval, combined with a

look-ahead algorithm, can be extended for use with the five-mode machine of the invention. At zero flow the machine is in a permanent idling mode. At low flows the operation sequence is composed of partial stroke and idling modes with the fraction of these two modes reflecting the demand level. As flow demand increases, the fraction of partial stroke modes relative to idling modes increases. At some stage the controller begins to use occasional full stroke modes interspersed with idle and part-stroke modes to continue the ramping up of flow. Starting from the other end of the range at full flow output, the machine is in permanent full stroke mode. As flow demand drops, idling modes are interspersed with full stroke modes, leaving regular gaps in the flow rate. This process continues until the ratio of full stroke modes to idling modes falls below a fixed or variable threshold, at which point the controller begins mixing idle modes, part stroke modes and full stroke modes. The mixture of modes of operation, where three modes are being employed in a sequence, is tailored for the smoothest flow result and/or the most seamless change in audible noise and/or minimal pressure ripple and/or optimum actuator motion. Several algorithms are possible to mix states over this range.

In the case of pressure control, the decision on the mixture of modes in the sequence is based upon some function of the error between the measured and demanded pressure, and optionally the time history of past system responses to past pumping/motoring decisions allowing for adaptive techniques to minimise pressure fluctuation in response to varying system parameters.

In the case of position or velocity control of an hydraulic actuator, the decision on the mixture of modes in the sequence is based upon some function of the error between the measured and demanded position or velocity, and optionally the time history of past system responses to past pumping/motoring decisions allowing for adaptive techniques to minimise position or velocity error in response to varying system parameters.

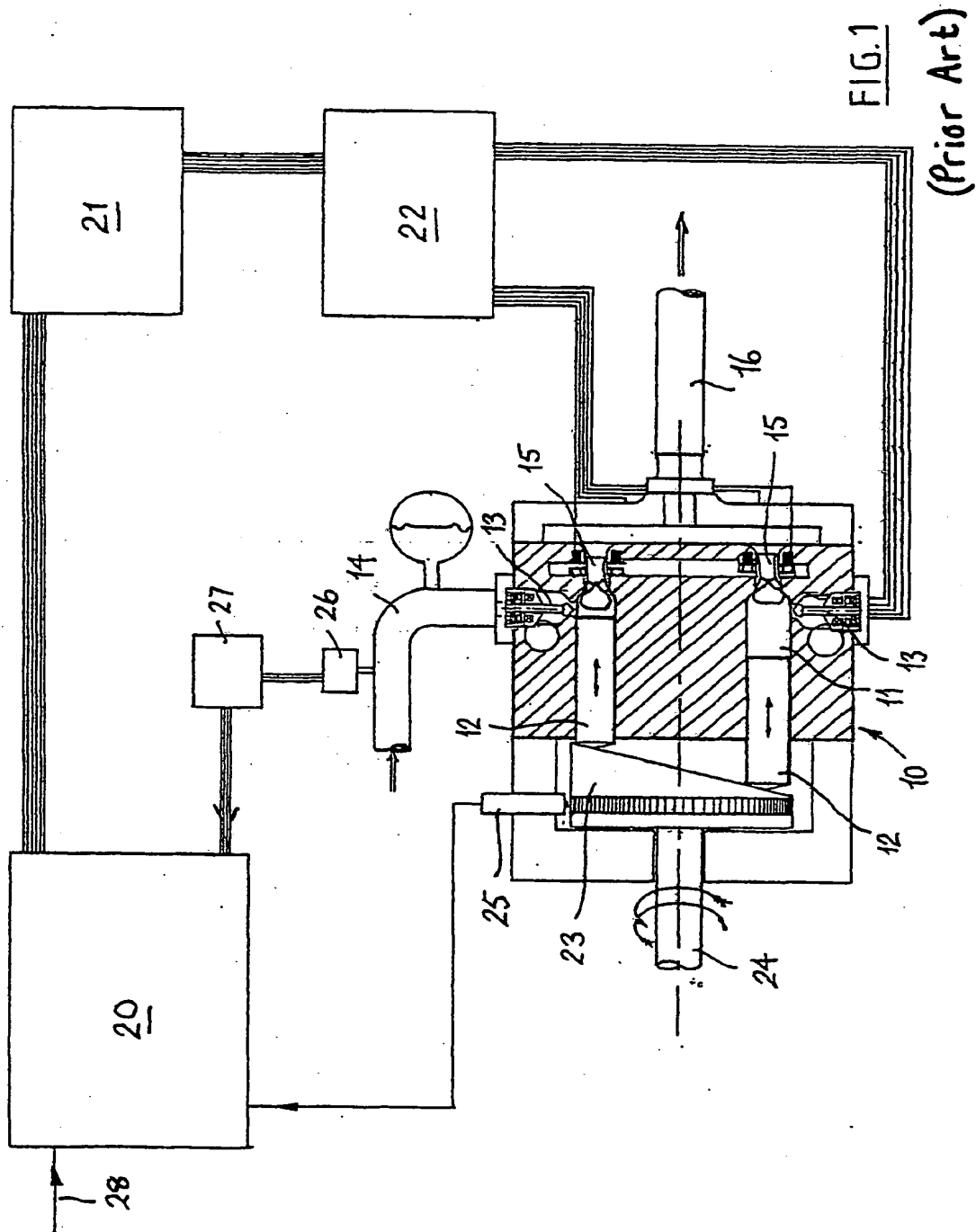
As alternatives to electromagnetic valves, valves operating by piezoelectric or magnetostrictive means could be used in the invention.

All forms of the verb "to comprise" used in this specification have the meaning "to consist of or include".

CLAIMS

1. A fluid-working machine having a plurality of working chambers of cyclically changing volume, a high-pressure fluid manifold and a low-pressure fluid manifold, at least one valve linking each working chamber to each manifold, and electronic sequencing means for operating said valves in timed relationship with the changing volume of each chamber, wherein the electronic sequencing means is arranged to operate the valves of each chamber in one of an idling mode, a partial mode in which only part of the usable volume of the chamber is used, and a full mode in which all of the usable volume of the chamber is used, and the electronic sequencing means is arranged to select the mode of each chamber on successive cycles so as to vary the time averaged effective flow rate of fluid through the machine.
2. A machine according to claim 1, wherein the partial mode comprises the use of only a small fraction of the usable volume of the chamber.
3. A machine according to claim 1 or 2, operable as both a pump and a motor, each chamber having five selectable modes, namely idling mode, partial motoring mode, full motoring mode, partial pumping mode and full pumping mode.
4. A machine according to claim 1, 2 or 3, wherein the working chambers comprise cylinders in which pistons are arranged to reciprocate.
5. A machine according to claim 4, wherein partial pumping mode includes closing the valve linking the cylinder to the low-pressure manifold and opening the valve linking the cylinder to the high-pressure manifold a small fraction in advance of the top dead centre position of the piston.
6. A machine according to claim 4, wherein partial motoring mode includes closing the valve linking the cylinder to the high-pressure manifold and opening the valve linking the cylinder to the low-pressure manifold a small fraction after the top dead centre position of the piston.

7. A method of operating a fluid-working machine having a plurality of working chambers of cyclically changing volume, a high-pressure fluid manifold and a low-pressure fluid manifold, at least one valve linking each working chamber to each manifold, comprising operating the valves of each chamber in one of an idling mode, a
5 partial mode in which only part of the usable volume of the chamber is used, and a full mode in which all of the usable volume of the chamber is used, wherein the mode of each chamber is selected on successive cycles so as to vary the time averaged effective flow rate of fluid through the machine.
- 10 8. A method according to claim 7, wherein the partial mode comprises the use of only a small fraction of the usable volume of the chamber.
9. A method according to claim 7 or 8, comprising selecting the number of chambers to be operated in each of said modes according to an algorithm depending on
15 the actual and required output of the machine.
10. A method according to claim 9, including a preliminary step of selecting whether to operate the machine as a pump or a motor, and choosing the algorithm accordingly.



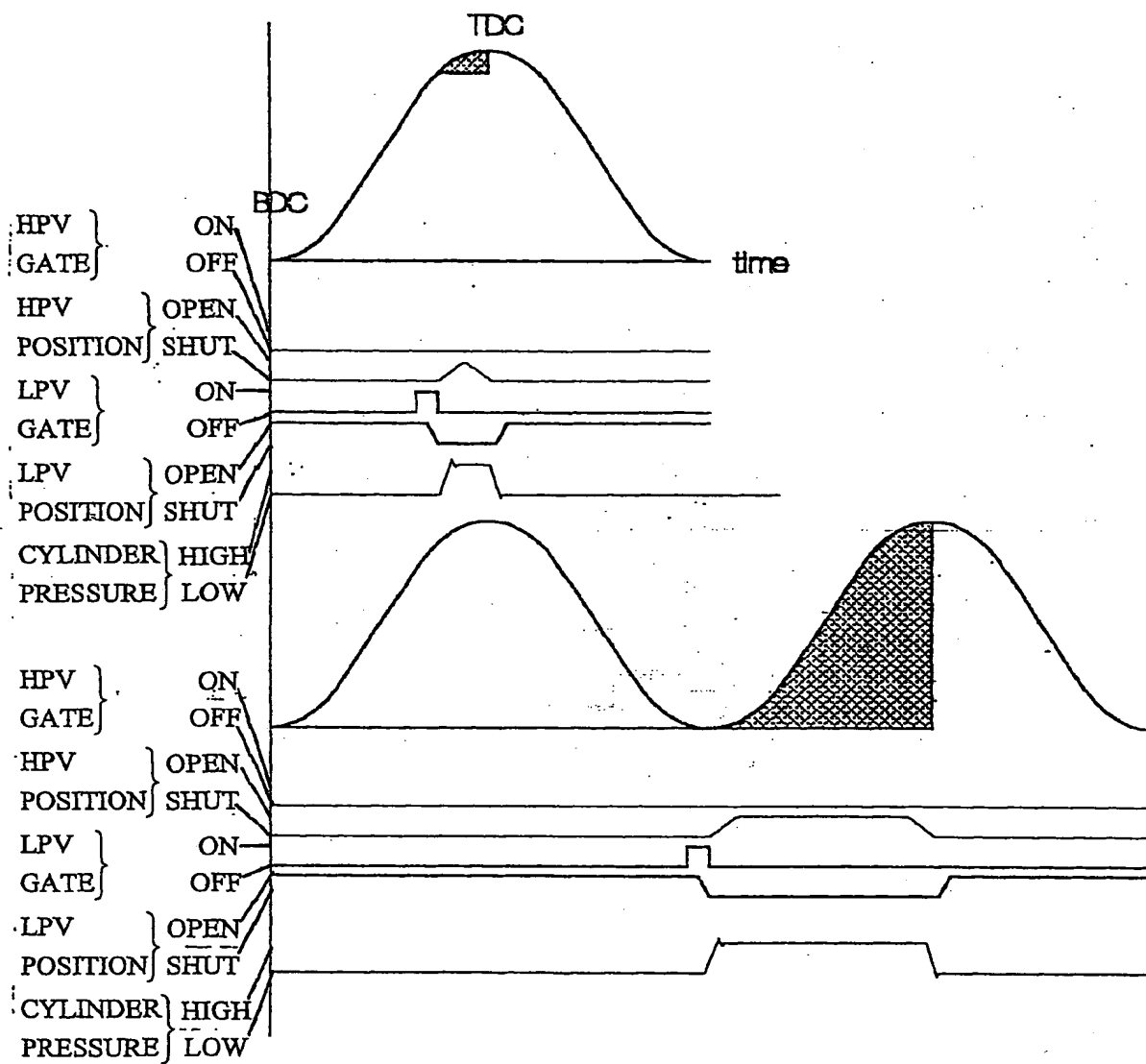


Fig. 2

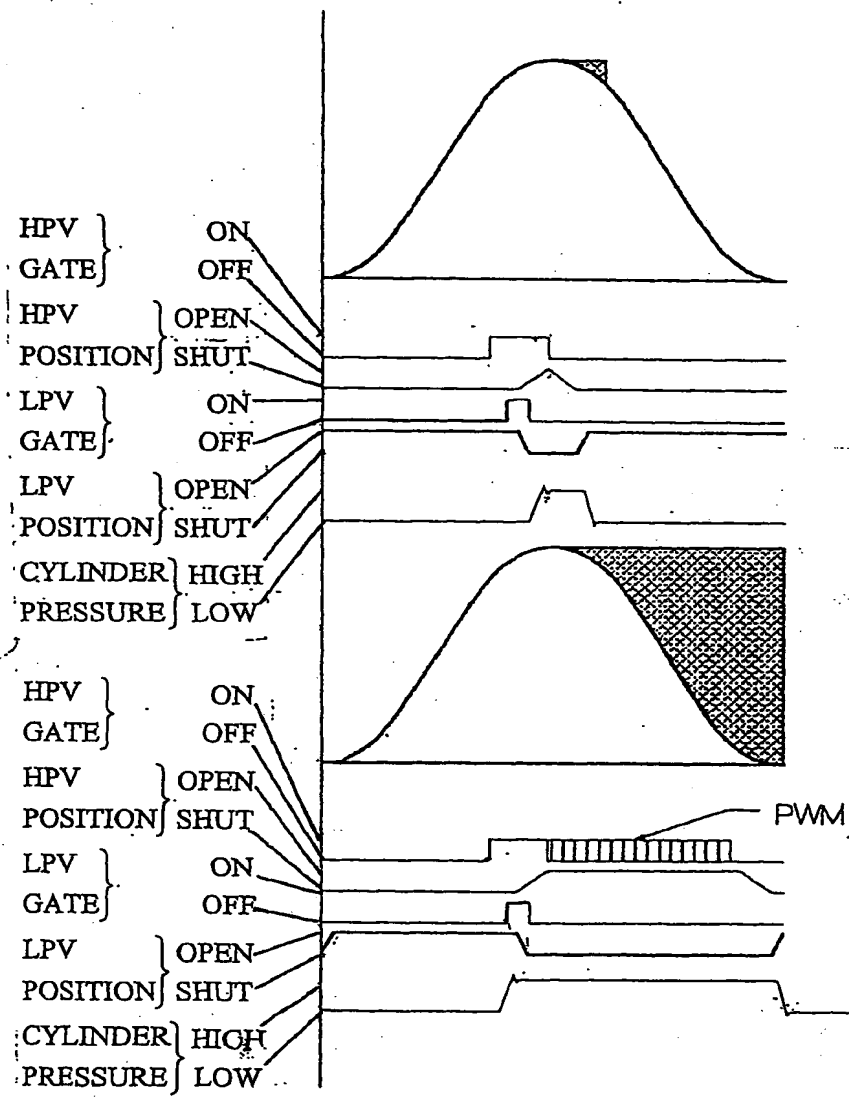


Fig. 3

INTERNATIONAL SEARCH REPORT

International Publication No
PCT/GB 03/03949

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 F04B49/06 F04B53/10 F04B7/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 F04B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 494 236 B (UNIV EDINBURGH) 15 July 1992 (1992-07-15) cited in the application column 2, line 4 -column 2, line 8 column 3, line 11 -column 4, line 12 column 6, line 8 -column 6, line 35 column 7, line 35 -column 7, line 42; claims 1,8; figures	1-10
A,P	EP 1 319 836 A (CATERPILLAR INC) 18 June 2003 (2003-06-18) column 9, line 50 -column 11, line 29 column 11, line 58 -column 12, line 14; figures 1,3	1-10
A	EP 0 501 463 A (NIPPON DENSO CO) 2 September 1992 (1992-09-02) abstract; figures 1,3,4	1-10

☐ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

* Special categories of cited documents:

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INTERNATIONAL SEARCH REPORT

Information on patent family members

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